

Basics of FE

1. $-u'' = f$ in $(0, 1)$ arbitrary weight

$$\frac{\partial^2 u}{\partial x^2} = -f \Rightarrow \int_{\Omega} w_p \frac{\partial^2 u}{\partial x^2} = - \int_{\Omega} w_p \cdot f$$

formula
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$$\Rightarrow \underbrace{\int_{\partial\Omega} w_p \frac{\partial u}{\partial x}}_{\text{boundary conditions}} + \int_{\Omega} \frac{\partial u}{\partial x} \frac{\partial w_p}{\partial x} = - \int_{\Omega} w_p \cdot f$$

for the Neumann case

Discretizing u as a sumation of shape functions, and imposing Galerkin ($w_p = N_p$), we obtain:

$$N_p \underbrace{\int_{\partial\Omega} \frac{\partial N_i}{\partial x} u_i}_{\text{boundary conditions}} \Big|_0^1 - \int_{\Omega} \sum_{i=1}^n \frac{\partial N_i}{\partial x} u_i \frac{\partial N_p}{\partial x} = - \int_{\Omega} N_p \cdot f$$

being u_i the FEE decomposition of u .

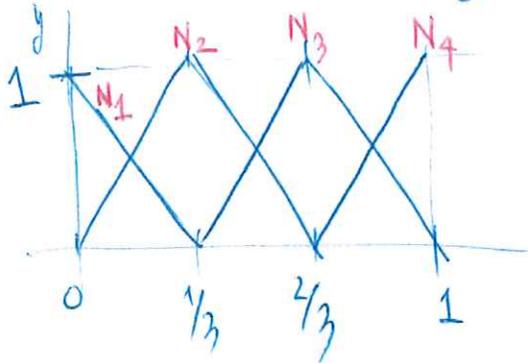
2) Developing the previous expression, we have the following structure: 2/3

$$\begin{array}{c} \boxed{\text{Boundary}} \\ \boxed{\text{Conditions}} \\ \boxed{\text{Dirichlet}} \end{array} + \left(\int \frac{\partial N_i}{\partial x} \cdot \frac{\partial N_j}{\partial x} \right) \cdot \begin{pmatrix} u_1 \\ \vdots \\ u_n \end{pmatrix} = \begin{pmatrix} \int N_i f \\ \vdots \\ \int N_i f \end{pmatrix}$$

$\underbrace{\hspace{10em}}_{\mathbf{K}} \quad \underbrace{\hspace{5em}}_{\mathbf{u}} \quad \underbrace{\hspace{5em}}_{\mathbf{f}}$

This is an standard system of equations with its appropriate boundary conditions.

3) We have the following shape functions:



$$N_1(x) = 1 - 3x$$

$$N_2(x) = \begin{cases} 3x & \text{in } (0, 1/3) \\ 2 - 3x & \text{in } (1/3, 2/3) \end{cases}$$

$$N_3(x) = \begin{cases} -1 + 3x & \text{in } (1/3, 2/3) \\ 3 - 3x & \text{in } (2/3, 1) \end{cases}$$

$$N_4(x) = -2 + 3x \quad \text{in } (2/3, 1)$$

So it is necessary to solve the following system of equations:

$$\begin{pmatrix} \int_0^1 N_1' N_1' & \int_0^1 N_2' N_1' & 0 & 0 \\ \int_0^1 N_2' N_1' & \int_0^1 N_2' N_2' & 0 & 0 \\ 0 & 0 & \int_0^1 N_3' N_3' & 0 \\ 0 & 0 & 0 & \int_0^1 N_4' N_4' \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{pmatrix} = \begin{pmatrix} \int_0^1 N_1(x) \cdot \text{sen}(x) dx \\ 0 \\ \vdots \\ \int_0^1 N_4(x) \cdot \text{sen}(x) dx \end{pmatrix}$$

(Sym)

B.B:

$$\begin{cases} u_1 = 0 \\ u_4 = 3 \end{cases}$$

Doing the necessary computations, we obtain:

$$\begin{pmatrix} 3 & -3 & 0 & 0 \\ -3 & 6 & -3 & 0 \\ 0 & -3 & 6 & -3 \\ 0 & 0 & -3 & 3 \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{pmatrix} = \begin{pmatrix} 0.0184 \\ 0.1080 \\ 0.2042 \\ 0.1290 \end{pmatrix}$$

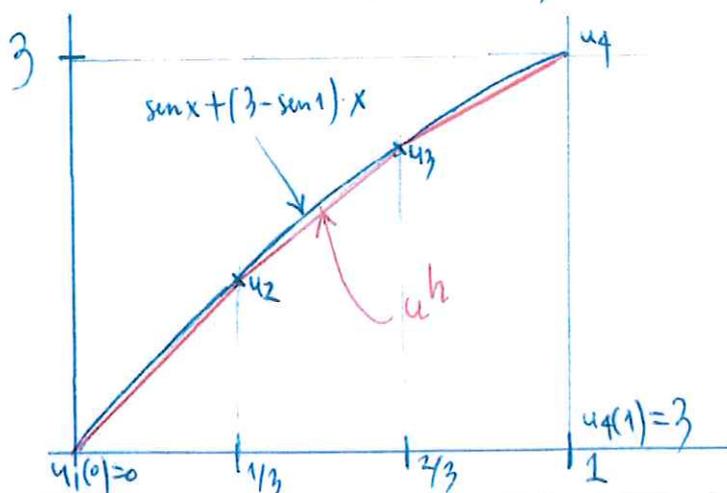
3/3

Eliminating both first and fourth files and columns and taking into account their boundary conditions information, we have:

$$\begin{pmatrix} 6 & -3 \\ -3 & 6 \end{pmatrix} \begin{pmatrix} u_2 \\ u_3 \end{pmatrix} = \begin{pmatrix} 0.1080 + 0 \\ 0.2042 + 9 \end{pmatrix}$$

u_1
B.C.
 $3u_4$

So, $\begin{pmatrix} u_2 \\ u_3 \end{pmatrix} = \begin{pmatrix} 1.0467 \\ 2.057 \end{pmatrix}$, and finally $\bar{u}^h = \begin{pmatrix} 0 \\ 1.0467 \\ 2.057 \\ 3 \end{pmatrix}$



Analytical and FEM approximation comparison

